

Figure 15. The whole experimental set-up

The FBG sensors were wired to an interrogator which was controlled using a personal computer. In order to sense the first to the third vibration modes, four sets of FBG were mounted at locations $x=8mm$, $x=90.4mm$, $x=159.3mm$ and $x=215.3mm$, respectively, to detect the strain signals. The positions of sensors were determined by the method presented in section III. A. Note that the first set was mounted at $x=8mm$ instead of $x=0mm$ due to the dimensions of gauges.

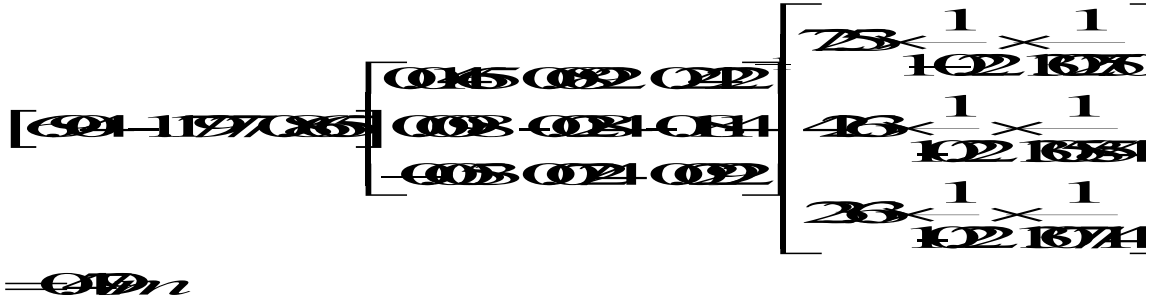
Assume that strain and deflection signals are composed of first-three modes, neglecting the

higher modes. The coefficient, listed in Table 2, is $\frac{\partial^2 Y_i(x_i)}{\partial x^2}$, come from mode shape analysis, by substituting these coefficient into Equation (22), we obtain the estimated displacement for the three modes.

Table 2 The physical and mechanical properties of the beam

	1# POINT	2#POSITION	3#POSITION
First mode	0.01465	0.0098	-0.0053
Second mode	0.0892	-0.0284	0.0724
Third mode	0.2422	-0.1814	0.0292

For example, when the cantilevered beam was excited by a harmonic force of 30 Hz, the FBG's strain response was $72.53\mu\epsilon$, $42.63\mu\epsilon$, $23.63\mu\epsilon$, respectively. The displacement of A point on beam (Figure.14) is:



The measurement error of beam tip can be obtained by an accelerator:

$$\frac{0.0011}{0.11} \times 10^{-8}$$

3. Experimental-2 set-up

Figure 16 shows an experimental rig for rotating beam, the beam, with four FBG mounted, is as same as section III.B. A motor drive a gearbox and the gearbox drive a shaft, the motor power is 45KW, the motor speed could change from 100 to 3000rpm from frequency control, the gearbox ratio is 1:5 and the maximum speed is 15000rpm. The beam is fixed the end of rotating shaft; the Figure 16 shows a close-up view of a rotary optical coupler using an optical circulator.

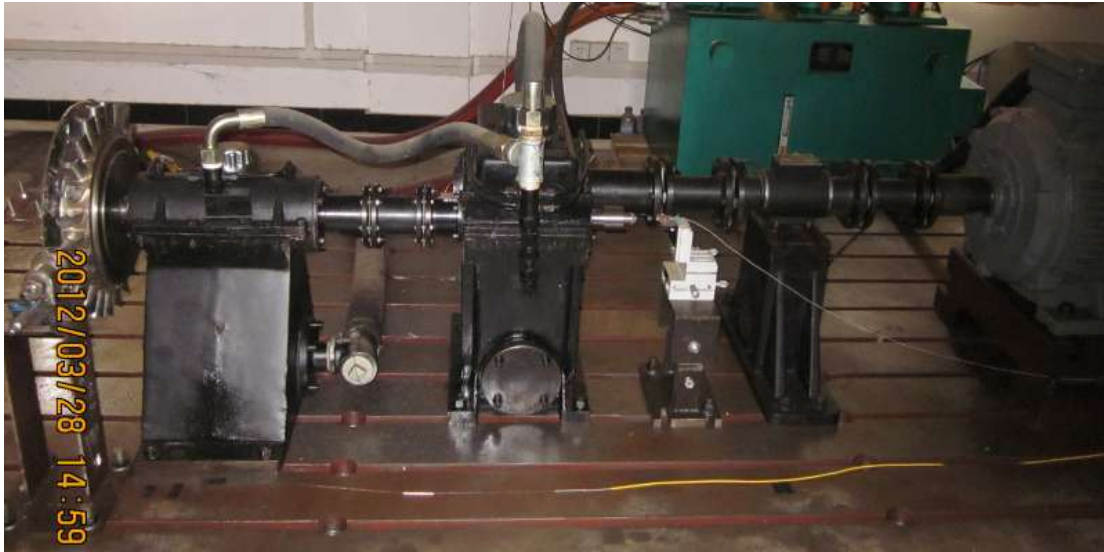


Figure 16. Experiment-2 set-up

IV. RESULTS AND DISCUSSION

A. Results

This section presents the results of strain measurements and an evaluation of displacement vibration of rotating a beam, by gradually increasing the rotational speed to 1200rpm and the 3-FBG's wavelengths were simultaneously recorded at a sampling rate of 2kHz.

Figure 17 shows micro strain of the FBG sensor mounted at 8mm of beam in range of 10-1200 rpm. Rotational speed was controlled by a motor controller. Rotational speed started at 10 rpm, at 10~15 second intervals, to 1200rpm at the end. From Figure 17, the dynamic strain shows oscillating vibration around a mean value. The mean strain decreases with rotational speed, which means the beam was stretched under centrifugal force. The oscillating vibration means that experiment was carried out under an elastic strain condition.

Figure 18 shows the measured dynamic strain against time at constant rotational speeds (approximately 325 rpm, with the same FBG sensor in Figure 17). The results of spectrum analysis show that 7.26 Hz, 14.53Hz, 55Hz cycles existed (Figure. 19). These means are doubled in frequency relating to rotating speed (7.26 Hz, 14.53Hz) and a frequency related to natural frequency of a cantilevered beam (55Hz, the simulation results is 60.199 Hz in section III, the difference came from the boundary condition).

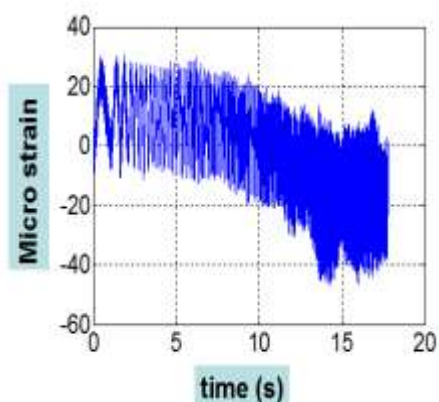


Figure 17 Strain on 1# FBG in range 0~900rpm

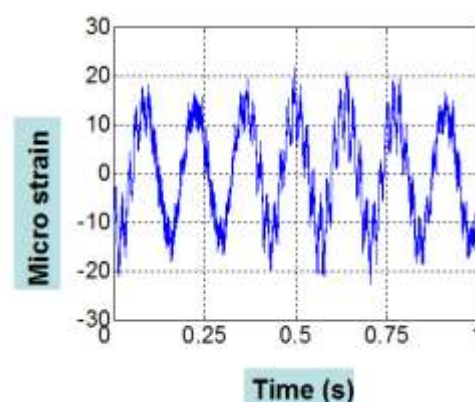


Figure 18 Strain on 1# FBG at 325rpm

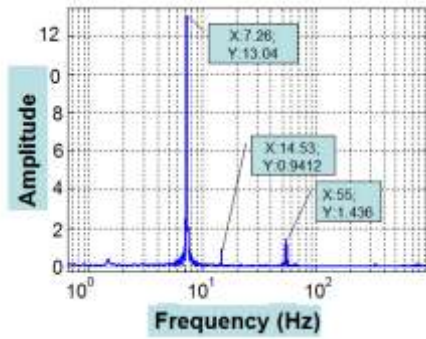


Figure. 19 Spectrum analysis of Figure 17

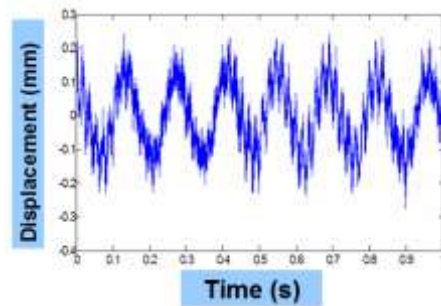


Figure. 20 The vibration estimation of the beam's tip

Figure 20 shows the vibration estimation of A point of beam at constant rotational speeds 325 rpm, blue line represent the case considering only the first three modes. From experimental-1, we know that the measurement error approximately 8.86%

B. Discussion

The errors came from the following causes.

- 1) The clamping condition of rotating cantilever beam does not yield a perfect fixed boundary condition.
- 2) The errors came from the FBG. Ideally, the sensors are moved to a more advantageous position. However, due to size of the FBG, the signals from the FBG are average values of a surface range. On the other hand, the sensitivity of the FBG is the source of the errors.
- 3) The relative error comes from the piezoelectric accelerometer which was used to calibrate the displacement vibration. To achieve higher displacement measurement, a sensor with higher sensitivity could be used.
- 4) 8.86% error is for consider only three. Due to measuring three modes there was an error of 8.86%. By taking more modes into account, errors will be reduced.
- 5) Since the location of the FBG is calculated based on analytical modes, it induced some errors.

V. CONCLUSIONS

The method of using an FBG to measure dynamic strain and estimate the displacement vibration of a rotating, cantilevered beam has been validated. This method is based on the fact that the vibration displacement can be expressed in terms of an infinite number of vibration modes and be related to the dynamic strains through the strain-displacement relationship. From the results, it can be concluded that this new monitoring method can be applied to a rotor blade.

REFERENCES

- [1] Southwell R, Gough F, “The free transverse vibration of airscrew blade”, British A.R.C. Reports and Memoranda, Vol. 766, 1921.
- [2] Nathan Rubinstein, James T. Stadter, “Bounds to bending frequencies of a rotating beam”, Journal of the Franklin Institute, Vol. 294, 1972, pp.217-229.
- [3] Putter S and Manor H. “Natural frequencies of radial rotating beams”, Journal of Sound and Vibration, Vol. 56, 1978; pp. 175-185.
- [4] S.V. Hoa , “Vibration of a rotating beam with tip mass”, Journal of Sound and Vibration, Vol. 72, 1979; pp. 369-381.
- [5] S.V. Hoa, D.H. Hodges, M.J. Rutkowski, “Comments on “vibration of a rotating beam with tip mass” ”, Journal of Sound and Vibration , Vol. 72,1980, pp.547-549.
- [6] Kuo, Tzung, Hurng Wu, Sen Yung Lee, “Bending vibration of a rotating non-uniform beam with tip mass and an elastically restrained root”, Computers & Structures, Vol. 42,1992:pp.229-236
- [7] T. Yokoyama, “Free vibration characteristics of rotating Timoshenko beams”, International Journal of Mechanical Sciences, Vol. 30, 1988; pp.743-755
- [8] H. H.Yoo, S. H.Shin, “Vibration analysis of rotating cantilever beams”, Journal of Sound and Vibration , Vol. 212, 1998,pp.807-828.
- [9] Shu, X., Liu, Y., Zhao, D, Gwandu, B., Floreani, F., Zhang, L.; Bennion, “Dependence of temperature and strain coefficients on fiber grating type and its application to simultaneous temperature and strain measurement”, Optics Letters, Vol. 27, 2002, pp.701-703.
- [10] Guru Prasad, A.S., “Measurement of stress-strain response of a rammed earth prism in compression using fiber bragg grating sensors”. International Journal on Smart Sensing and Intelligent Systems, September 2011, pp 376-387,
- [11] S. Bhalla , Y.W. Yang , J. Zhao, C.K. Soh. “Structural health monitoring of underground facilities-Technological issues and challenges”, Tunnelling and Underground Space Technology, Vol. 20, 2005, pp.487-500

[12]Kyungmok Kim, Jong Min Lee, Yoha Hwang, “Determination of engineering strain distribution in a rotor blade with fibre Bragg grating array and a rotary optic coupler” *Optics and Lasers in Engineering*, Vol. 46, 2008, pp.758-762.

[13]Chen-Jung Li and A. Galip Ulsoy, “High-Precision Measurement Of Tool-Tip Displacement Using Strain Gauges In Precision Flexible Line Boring”, *Mechanical Systems and Signal Processing*, Vol. 13(4), 1999, pp.531-546

[14]G. Pavic, “Measurement of vibrations by strain gauges, Part I: theoretical basis”, *Journal of Sound and vibration*, Vol. 102, 1985, pp.153~163.